Current State of Military Hybrid Vehicle Development by Denise M. Kramer, U.S. Army RDECOM-TARDEC Gordon P. Parker, Michigan Technological University

Abstract

Hybrid vehicles are common in the marketplace for passenger cars and commercial applications such as delivery trucks and transit busses. One of the biggest justifications for hybrids is their fuel efficiency. With fuel costs as high as \$100 per liter in the battlefield it is remarkable that there are no deployed hybrid military vehicles. This is not due to a lack of investment in research and development, since much work has been done. The goal of this survey paper is to summarize past research in both the commercial and government sectors towards achieving a military hybrid vehicle and provide recommendations for a path forward. Special attention is given to drive cycles and the unique requirements that impact military hybrid vehicle design.

Introduction

With ever increasing emission and fuel economy requirements in the U.S., Europe and Asia, most of the passenger car (defined as 3,850 kg or less) Original Equipment Manufacturers (OEMs) have conducted extensive research on various types of hybrid vehicles to comply with these new demands. The literature illustrates not only research, but includes product development, which demonstrates that most of the OEMs in Europe and the Americas have a hybrid model in the marketplace or will introduce one in the near future [1]. Furthermore, the use of hybrid powertrain components consisting of power electronics and electric motor drives have established themselves as a means of improving the energy efficiency of passenger cars [1]. Additionally, there has been significant progress in the development of hybrid transit busses worldwide [2], which also shows that energy savings can be realized with hybrid powertrains. This work has also been extended to delivery trucks and garbage trucks, which have a similar application that utilizes the same type of drive cycle.

Militaries worldwide are also interested in realizing the potential energy savings from utilizing hybrid vehicles. "Fossil fuel accounts for 30 to 80 percent of the load in convoys into Afghanistan, bringing costs as well as risk. While the military buys gas for just over \$1 a gallon, getting that gallon to some forward operating bases costs \$400," according to Gen. James T. Conway, the commandant of the U.S. Marine Corps [3]. In fact, the U.S. Army has been researching hybrid vehicles since 1943[4]. However, from observing the literature, it appears that the U.S. and other countries are further away from realizing a hybrid ground vehicle. There are very few if any hardware related papers and many of the papers overlook some of the basic requirements of military ground vehicles, such as 60% grade ability and fording. The lack of literature related to European and Asian military vehicles conveys that armies worldwide are also facing the challenge of fielding a hybrid military vehicle. Furthermore, a standard or universally accepted duty cycle for measuring fuel economy does not exist nor does a focus towards a particular technology. This could be for the following reasons:

- (1) Military ground vehicle researchers do not publish as readily as OEM researchers, due to lack of available data, test vehicles and proprietary information.
- (2) The challenge of a military application is much greater due to the ever increasing and mutating threats that translate into continually changing requirements.
- (3) The life cycle of military vehicles is much different than that of passenger vehicles and not enough development has been completed to understand the long-term reliability and maintainability of hybrid components.

Report Docume	entation Page	Form Approved OMB No. 0704-0188	
Public reporting burden for the collection of information is estimated to maintaining the data needed, and completing and reviewing the collect including suggestions for reducing this burden, to Washington Headqu VA 22202-4302. Respondents should be aware that notwithstanding ar does not display a currently valid OMB control number.	ion of information. Send comments regarding this burden estimate arters Services, Directorate for Information Operations and Reports	or any other aspect of this collection of information, s, 1215 Jefferson Davis Highway, Suite 1204, Arlington	
1. REPORT DATE 2. REPORT TYPE 31 AUG 2011 Journal Article		3. DATES COVERED 31-08-2011 to 31-08-2011	
4. TITLE AND SUBTITLE		5a. CONTRACT NUMBER	
CURRENT STATE OF MILITARY H DEVELOPMENT	IYBRID VEHICLE	5b. GRANT NUMBER	
DEVELOPMENT		5c. PROGRAM ELEMENT NUMBER	
6. AUTHOR(S)		5d. PROJECT NUMBER	
Denise Kramer; Gordon Parker		5e. TASK NUMBER	
		5f. WORK UNIT NUMBER	
7. PERFORMING ORGANIZATION NAME(S) AND AD U.S. Army TARDEC ,6501 E.11 Mile I	· · ·	8. PERFORMING ORGANIZATION REPORT NUMBER #22263	
9. SPONSORING/MONITORING AGENCY NAME(S) A U.S. Army TARDEC, 6501 E.11 Mile I		10. SPONSOR/MONITOR'S ACRONYM(S) TARDEC	
		11. SPONSOR/MONITOR'S REPORT NUMBER(S) #22263	
12. DISTRIBUTION/AVAILABILITY STATEMENT Approved for public release; distribution	on unlimited		
13. SUPPLEMENTARY NOTES			
Hybrid vehicles are common in the madelivery trucks and transit busses. One fuel costs as high as \$100 per liter in the military vehicles. This is not due to a labeen done. The goal of this survey paper government sectors towards achieving forward. Special attention is given to divehicle design.	e of the biggest justifications for hybra he battlefield it is remarkable that the nck of investment in research and de her is to summarize past research in b a military hybrid vehicle and provid	rids is their fuel efficiency. With ere are no deployed hybrid velopment, since much work has both the commercial and le recommendations for a path	
15. SUBJECT TERMS			

c. THIS PAGE

unclassified

16. SECURITY CLASSIFICATION OF:

b. ABSTRACT

unclassified

a. REPORT

unclassified

17. LIMITATION OF

ABSTRACT

Same as

Report (SAR)

18. NUMBER

OF PAGES

17

19a. NAME OF RESPONSIBLE PERSON (4) The off-road mobility requirements present a unique challenge and off-road production hybrid vehicles are only recently starting to emerge in the construction equipment sector.

To understand what has been accomplished and where the challenges are, this paper will summarize the current state of the art, the missing pieces and suggest future directions to aid development of military hybrid ground vehicles.

Background on Research

For fifty years, the U.S. military has been considering the use of electric drive technology [5]. To understand the performance of this technology the Hybrid-Electric Vehicle Experimentation and Assessment (HEVEA) program was initiated in 2005 [5]. The goals of this program were to understand how hybrids performed in a military environment, establish a test procedure for evaluating their performance and create a validated simulation tool for evaluating system-level performance [5, 6]. During the course of this program various one-off hybrid vehicles were developed and tested:

- XM1124 High Mobility Multipurpose Wheeled Vehicles (HMMWV) Series Electric
- Future Tactical Truck Systems (FTTS) Parallel Electric
- Family Medium Tactical Vehicle (FMTV) Hydraulic Hybrid
- Family Medium Tactical Vehicle (FMTV) Series Electric
- Heavy Mobility Expanded Tactical Truck (HEMTT) Series Electric

With the introduction of the Future Combat Systems (FCS) program, a series of conference papers were published [7-15, 44, 48] by various OEMs to show capability on current vehicles using OEM specific hardware. Some of the prototype hybrid vehicles developed under the FCS program were:

- EP-50 Parallel Hybrid Light Armored Vehicle (LAV-III) and a Refuse Hauler
- Advanced Hybrid Electric Drive (AHED) 8x8, 20 ton Series Hybrid (new start)
- Hybrid Electric (HE) M113 Series Hybrid
- Family Medium Tactical Vehicle (FMTV) Hydraulic Hybrid
- Commercially Based Tactical Truck (COMBATT) Dodge RAM Hybrid

Additionally, the commercial sector has shown success with hybrid systems for heavy duty vehicles that have a known drive cycle such as city busses and delivery trucks. Some examples include:

- Allison Hybrid EP System[™] Transit buses two-mode parallel hybrid with continuously variable transmission (CVT)
- Azure Balance Hybrid™ Ford E-450 chassis parallel hybrid post transmission with starter/generator
- BAE HybridDrive [™] Series Hybrid Electric with a fixed gear reduction
- Eaton Parallel Hybrid Electric integrated motor/generator with automatic transmission

Currently, the three technology demonstrators for the U.S. Army's Joint Light Tactical Vehicle (JLTV) all have Integrated Starter Generators (ISGs), which are not used for propulsion, but could be expanded into mild hybrid capability with the addition of a clutch connecting the generator to the transmission and additional energy storage [16-17]. Additionally, the U.S. Army's Fuel Economy Demonstrator (FED) program is creating two demonstrators: one with an ISG only and one that is a full parallel electric hybrid [18-21].

Military Challenges

As illustrated above, there has been years of work with respect to U.S. military hybrids, however, there has not been a military HEV fielded to date. A paper published in 2009, explains in detail the challenges

that military vehicles face [4]. In summary, the vehicle performance requirements such as 60% grade ability, speed on grade, cooling and soft soil mobility add challenges that could diminish the gains seen by a hybrid vehicle. In addition, their reliability and maintainability is unknown for the lifecycle of a military vehicle. Lastly, the continuously changing threat impedes engineers from understanding the duty cycle and use of the vehicle. However, as technology is ever advancing and hybrids are becoming mainstream for commercial applications including some heavy duty vehicles, such as busses and delivery trucks, it appears that these technologies could be leveraged to eventually field hybrid military vehicles.

Opportunity

It is generally accepted that hybrids can provide improved fuel economy, in fact, a study conducted in 1999 concluded that by just considering an engine fuel map and eliminating the inefficiencies associated with idling, vehicle braking and low engine speed part load efficiency, many improvements could be realized as shown in Table 1 [22].

Vehicle	Vehicle Class	Fuel Economy Improvement	Cycle
Ford E-Super Duty Truck	III	61%	Average over Central Business District (CBD), New York City Bus Cycle and Commute Phase Truck Cycle (COMM)
GMC C-Series P-Chassis Truck	III	75%	Average over Central Business District (CBD), New York City Bus Cycle and Commute Phase Truck Cycle (COMM)
Navistar 300 Series Bus	VI	35%	Average over Central Business District (CBD), New York City Bus Cycle and Commute Phase Truck Cycle (COMM)

Table 1: Fuel savings for Class III and IV trucks predicted by the study of Reference 22.

A vehicle's class is defined by its gross vehicle weight (GVW) summarized below [47].

- (1) Medium Duty:
 - Class III 4,536-6,350 kg
 - Class IV 6,351-7,257 kg
 - Class V 7,258-8,845 kg
- (2) Heavy Duty:
 - Class VI 8,846-11,793 kg
 - Class VII 11,794-14,969 kg
 - Class VIII 14,970 kg +

While this work does not take into account component integration or optimal controls, Table 1 shows the potential for medium and heavy duty vehicles.

The study by Stodolsky et al. [23] showed that class III – IV trucks can obtain an average of 93% fuel economy gains over a number of urban / city cycles while class VI – VII trucks can obtain an average of 71% over the same cycles. As illustrated by these two papers, hybrids show promise in regard to fuel economy savings. Therefore, the next sections will introduce the military vehicles and drive cycles used

as well as summarize fuel economy improvements that have been shown in the literature according to the powertrain configuration used, parallel and series.

Vehicle Overview

While many different vehicles are used in the battlefield worldwide, there are only three different military vehicles used for all of the publications: HMMWV, shown in Figure 1, FMTV, shown in Figure 2, and HEMMTT, shown in Figure 3. However, these three vehicles span a wide range of weights from 4,536 to 14,970+ kg indicative of class III through class VII vehicles. Furthermore, information and data related to these vehicles are readily available.



Figure 1: High Mobility Multipurpose Wheeled Vehicles (HMMWV)



Figure 2: Family Medium Tactical Vehicle (FMTV)



Figure 3: Heavy Mobility Expanded Tactical Truck (HEMMTT)

Drive Cycle Overview

To determine fuel economy improvement it is necessary to test a vehicle or run a simulation over a specified drive cycle. A review of the literature showed that many different drive cycles were being used to evaluate vehicle performance. These cycles can be divided into the following two categories:

- (1) Time dependent speed profiles, shown in Figure 4, usually defined by the federal government (EPA) [42]:
 - FTP 75 Cycle
 - Urban Cycle
 - Highway Cycle

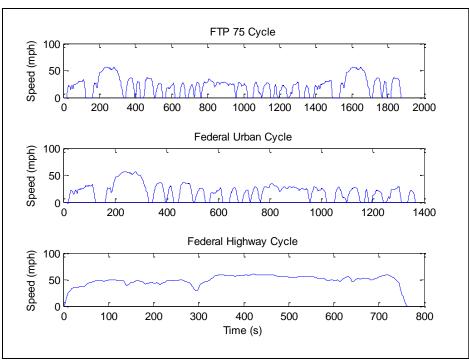


Figure 4: Time Dependent Speed Profiles

- (2) Distance dependent grade or elevation profiles (figure 5, below) usually defined by the U.S. Army:
 - Churchville Cycle
 - Harford Cycle
 - Munson Cycle

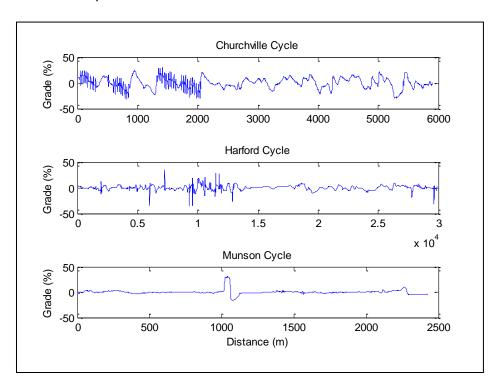


Figure 5: Distance Dependent Grade Profiles

In general, hybrid vehicle fuel savings are realized when the vehicle undergoes frequent speed or load changes. A qualitative examination of Figures 4 and 5 shows that the FTP75, Federal Urban, Churchville and Hartford cycles all have significant speed or load frequency content. Conversely, the Federal Highway and Munson cycles have very few speed or load changes. The influence of these different drive cycles will be further analyzed in the drive cycle impact section.

Parallel Powertrain

A parallel hybrid powertrain is a configuration where both the internal combustion engine and another power source can drive the wheels. The other power source can be an electric motor or a hydraulic accumulator. The system is described by the term parallel because the power to move the vehicle can come from two different paths. A detailed description of the different powertrain versions are explained in references 24-27. Table 2 gives a summary of fuel economy improvements reported in the literature for parallel hybrid systems, which include mild, electric and hydraulic. Additionally, the vehicles are sorted from lightest to heaviest for each section and most to least fuel economy improvement. It is important to note for many of the configurations a fuel economy improvement range was reported with only the maximum improvement shown in Table 2. Therefore, the values reported in Table 2 are the 'best case' or maximum value that could be attained.

Parallel Type	Vehicle	Vehicle Class	Cycle	Fuel Economy Improvement	Method	
Mild	HMMWV	III	Composite	4.3%	Integrated starter generator for engine shut down, regenerative braking and avoidance of inefficient engine operation [28].	
Σ	∑ FMTV VI		Composite	6-9%	Fuel cell advance power unit to allow for engine shut down [29].	
	HMMWV III		Urban, Highway, Composite	21%, 35.8%, 26.5%	Parallel electric hybrid vehicle [30].	
		HMMWV III		Urban	18%	Engine in the loop simulation with stochastic dynamic programming control system optimizing for fuel economy and emissions [31].
			MMWV III		17.8%, 45.2%	Simulation using optimal design and power management system [32].
				Munson, Churchville B	7%, 11.3%	Series - Parallel hybrid with a continuously variable transmission using optimal design and power management system [31].
ectric	IIV VTM4	FMTV VI			2%, 16.7%	Simulation using optimal design and power management system [31].
E				-5%, 30%	Series - Parallel hybrid with a continuously variable transmission using optimal design and power management system [31].	
			Munson, Churchville B	7.5%, 11.5%	Simulation using optimal design and power management system [31].	
				11.9%, 15.4%	Series - Parallel hybrid with a continuously variable transmission using optimal design and power management system [31].	
	HEMMTT VIII			2.9%, 0%	Series - Parallel hybrid with a continuously variable transmission using optimal design and power management system [31].	

			0%, 0%		Simulation using optimal design and power management system [31].
draulic	Composite	Composite	32%	Simulation using optimal design (2/3) and dynamic programming power management system [33].	
Ť			Urban	26.7%	Hydraulic hybrid vehicle testing [34].

Table 2: Summary of published fuel economy benefits of three types of parallel hybrid powertrain configurations for Class III, VI, VII, and VIII vehicles. Shading indicates a prototype study. All others were simulation only.

In summary, a Class III HMMWV can realize between 4.3 – 45.2% fuel economy improvement depending on technology and drive cycles, whereas the Class VI and VII FMTV can realize between 2-32% and 7-15% respectively. Lastly, the Class VIII HEMMTT only demonstrates an improvement between 0 - 2%. The results of these studies indicate that for parallel hybrid powertratins there exists more opportunity for smaller Class vehicles

As noted earlier, many different drive cycles were used in the studies for these vehicles ranging from a combinations of courses that were intended to represent military driving conditions, to Munson and Churchville courses, which are test courses from the U.S. Army Aberdeen Proving Grounds, to standard courses developed by the U.S. government to test passenger cars and heavy duty trucks. A detailed discussion on drive cycles is given in drive cycle impact section.

Lastly, a majority of the papers – all but the two shaded entries of Table 2 – focus on simulation. Very few military hybrid vehicle prototype studies have been published, which could be due to proprietary information or simply a lack of hardware development.

Series Powertrain

A series powertrain is where the internal combustion engine drives a second power source, which drives the wheels of the vehicle. The second power source can be an electric motor or a hydraulic accumulator. The system is called a series system because the power flows on one path in a serial fashion. A detailed description can be found in references 24-27. Table 3 gives a summary of fuel economy improvements reported in the literature for series hybrid systems, which include electric and hydraulic. As in the previous section, the vehicles are sorted from lightest to heaviest for each section and most to least fuel economy improvement. Again, the range of fuel economy improvements was reported and the maximum improvement was chosen for the summary in Table 3. Therefore, the values reported in Table 3 can be considered the 'best case' or maximum value that could be attained.

Series Type	Vehicle	Vehicle Class	Cycle	Fuel Economy Improvement	Method
			Urban	49.6%	Simulation with two sliding mode base controllers - one for engine speed control and one for engine/generator torque [35].
ectric	III vwwwh	III	Urban, Highway, Composite	33%, 27.9%, 49%	General vehicle simulation [30].
Ele			Urban	19.0%	Simulation and prototype testing of the XM1124 [36].
			Munson, Churchville B	12.1%, 43.5%	Simulation using optimal design and power management system [31].

				7%, 11.3%	Series - Parallel electric hybrid with a continuously variable transmission using optimal design and power management system [31].
	Notional Military Bus	VI	Four different Urban Cycles	19.1%, 15.9%, 22.7%, 12.5%	Simulation using parametric design and an energy management for fuel economy [37].
			Urban	7.1%	Simulation optimized for fuel economy with 60% grade and acceleration constraints [38].
	FMTV	VI		-5.9%, 30%	Simulation using optimal design and power management system [31].
				-5%, 30%	Series - Parallel electric hybrid with a continuously variable transmission using optimal design and power management system [31].
	FMTV	VII	Munson, Churchville B	11.9%, 15.4%	Series - Parallel electric hybrid with a continuously variable transmission using optimal design and power management system [31].
				-1.5%, 19.2%	Simulation using optimal design and power management system [31].
	LIED AD ATT	V /II		17.4%	Vehicle simulation without batteries designed using target cascading [39].
	HEMMTT	VII	Composite	12.5%	Electric vehicle simulation without batteries designed using target cascading [39].
			15.8%	Vehicle simulation without batteries designed using target cascading [39].	
	НЕММТТ			15.6%	Simulation with in-hub wheel motors designed using target cascading [39].
			2.9%, 0%	Series - Parallel hybrid with a continuously variable transmission using optimal design and power management system [31].	
				0%, 9.1%	Simulation using optimal design and power management system [31].
Hydraulic	HMMWV	III	Urban, Highway	68%, 12%	Simulation with optimized supervisory control [40].
Нуд	FMTV	VI	Composite	20%	General vehicle simulation [41].

Table 3: Summary of published fuel economy benefits of two types of series hybrid powertrain configurations for Class III, VI, VII, and VIII vehicles. Shading indicates a prototype study. All others were simulation only.

In summary, a HMMWV can realize between 7-68% fuel economy improvement depending on its technology and drive cycles, where the FMTV can realize between -5.9-30% and -1.5-19.2% for class VI and VII, respectively. The HEMMTT can demonstrate between 12.5-17.4% and 0-15.8% improvement for class VII and VIII, respectively. Last, a notional military bus (class VI) shows a 12.5%-19.1% improvement, again depending on drive cycle and technology. The series hybrid analysis as with the parallel hybrid demonstrates that there is the greatest opportunity with lighter vehicles. However, the series hybrid shows more potential for improvement in the very large class VII-VIII vehicles than a parallel hybrid.

As with the earlier section, the HMMWV, FMTV and HEMMTT were used for all of the analyses with the exception of the study of reference 37 that used a notional military bus. All of the studies were simulation only with the exception of one (shaded, reference 36). Finally, many different drive cycles were used and a discussion is detailed in the next section.

Fuel Economy Improvement vs. Drive Cycle

To further understand the effect of drive cycles, figure 6 shows cycle versus percent fuel economy improvement for series, parallel and series-parallel combination for the class III HMMWV vehicle based on the results provided in references 28, 30, 31, 32, 35, 36, and 40. While the configuration and methods were different for each of the points on the plot, a general trend shows that the hybrid HMMWVs show more improvement on urban cycles, which is expected. Furthermore, vehicles tested on the Munson cycle show the least amount of fuel economy improvement, which is also anticipated since the Munson drive cycle is nearly a flat course without any stops as shown in Figure 5.

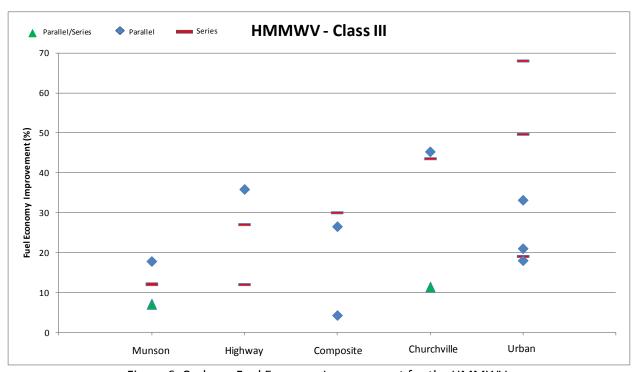


Figure 6: Cycle vs. Fuel Economy Improvement for the HMMWV

Figure 7 is a similar plot for Class VI vehicles where the data is extracted from references 29, 31, 33, 34, 37, 38, and 41. In this plot, a composite cycle is a catch-all bin for ad-hoc cycles. Once more, the urban cycle shows the most improvement, while the Munson cycle shows a degradation in fuel economy in some cases.

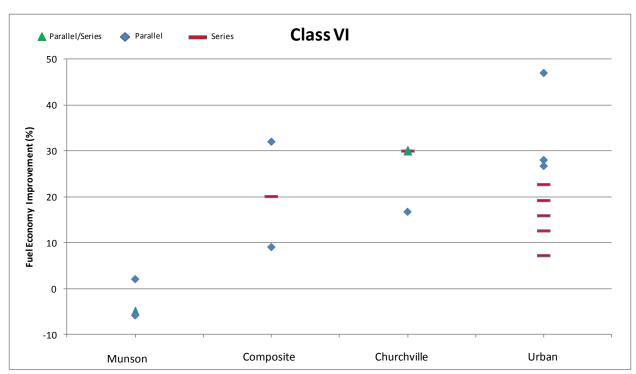


Figure 7: Cycle vs. Fuel Economy Improvement for the Class VI Vehicle

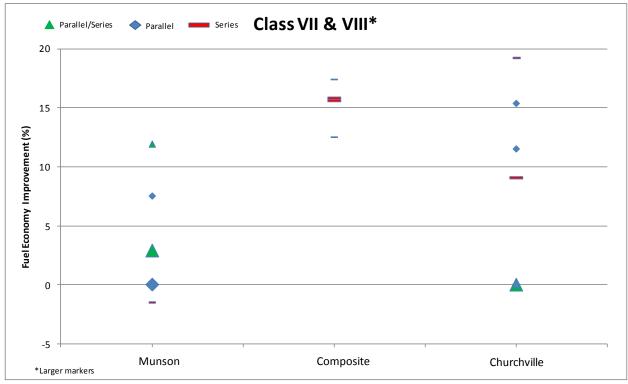


Figure 8: Cycle vs. Fuel Economy Improvement for the Class VII & VIII Vehicle

Figure 8 shows the drive cycle versus fuel economy improvement for Class VII and VIII vehicles from references 31 and 39. Since an Urban cycle was not used in either of these publications, Churchville,

which has some characteristics of an urban cycle, showed the best results. Again, Munson showed the least improvement.

It is important to note that work has been done [45] to develop a true military combat drive cycle to understand operational fuel economy. This study used a motion simulator with soldiers-in-the-loop facing military scenarios, such as a convoy escort mission, to determine typical speed and load profiles that could be used for a drive cycle. Based on the surveyed literature, these cycles have not been adopted by the community.

In summary, the fuel economy improvement for military hybrid vehicles is highly dependent on the drive cycle used for the analysis. The existing literature shows the lack of a standard drive cycle for analysis, which makes it difficult to judge technologies and understand how the military can benefit from a hybrid vehicle. This is likely one of the reasons for the delay in fielding a military hybrid.

Other capabilities

While this paper focuses on fuel economy improvements for military hybrid vehicles, it is important to note that there are other potential payoffs. The first benefit is the ability to idle and possibly move without the noise and thermal signatures of its internal combustion engine [5]. Another benefit is the increased onboard electrical power for auxiliary equipment. Not only can a hybrid system, such as an engine with an integrated starter generator, provide more electrical power than the typical alternator, but this power can be converted, conditioned and delivered in any form to and from any load. Some examples included charging the soldiers' batteries or delivering power back into an electrical grid. Additionally, new military vehicles are demanding an excess of 50kW [49], which can only be provided with an advanced onboard power unit or a hybrid system. Quantifying these capabilities could help governments understand the benefits of military hybrid vehicles.

Constraint gaps

Military vehicles typically have clear requirements with regard to grade ability, acceleration levels and speed on grade. These requirements will differ from commercial or passenger vehicles and for the different class of vehicles; however, the literature shows that a standard set of requirements is not being used. Fuel economy will be adversely affected when trading off acceleration or grade performance; therefore, it is difficult to determine comparable fuel economy performance across studies using different requirements.

Table 5 summarizes the fuel economy improvements for the Class III HMMWV over the urban cycle with different grade and performance requirements used for the analyses of references 30, 31, 35, 36 and 40. For each of the studies, a different standard was used for grade or acceleration. In three cases, no information was given regarding these requirements. According to the Hybrid Electric HMMWV specification [46] the HMMWV at gross vehicle weight (GVW) shall:

- Be capable of starting and stopping on slopes up to and including 60%.
- Be capable of ascending a 5% grade at 55 mph.
- Accelerate from 0 to 30 mph within 9.0 seconds and from 0 to 50 mph within 24 seconds.

Vehicle	Acceleration	Grade	Fuel economy improvement
Series Electrical	none	none	49.6%
Series Electrical	0-60mph: 16.5s	3.2% grade @ 20mph	33.0%

Series Electrical	none	none	19.0%
Series Hydraulic	0-50mph: 10.8s	2% grade @ 55mph, 3% grade @ 45mph	68.0%
Parallel Electric	0-60mph: 21.7s	0% grade @ 20mph	21.0%
Parallel Electric	none	none	18.0%

Table 5: Summary of HMMWV Urban Cycle Performance and Requirements

The analysis summarized by Dususin et el. [43] noted that 60% grades are achievable, but this type of driving cycle will push motors in a series system to their peak power and the motors can only maintain peak power for a short amount of time. This indicates that the 60% grade constraint is one of the challenging requirements in the design of a military hybrid vehicle.

The study in reference 38 used the 60% grade as a constraint in the optimization for a series electric FMTV Class IV vehicle where the fuel economy improvement was predicted to be 7.1% over the urban cycle, which is the smallest improvement for the Class IV over the urban cycle of all the studies considered in Tables 3 and 4. The analysis conducted in reference 31 makes note that all of the vehicle configurations used in their simulations match current acceleration and grade performance targets, but does not provide further details.

Table 6 contains a similar summary for the FMTV Class IV vehicle. The results are similar to the HMMWV where there is an absence of standard performance requirements.

Vehicle	Acceleration	Grade	Fuel economy improvement
Series Electrical	0-37.2mph: 22s	Traverse 25% grade	19.1%
Series Electrical	0-37.2mph: 22s	Traverse 25% grade	15.9%
Series Electrical	0-37.2mph: 22s	Traverse 25% grade	22.7%
Series Electrical	0-37.2mph: 22s	Traverse 25% grade	12.5%
Series Electrical	0-50mph: 25s	Traverse 60% grade	7.1%
Parallel Hydraulic	none	none	26.7%
Parallel Electric	none	none	28.0%
Parallel Hydraulic	none	none	47.0%

Table 6: Summary of FMTV Class IV Urban Cycle Performance and Requirements

Summary

Many studies have shown that hybrid powertrains can yield fuel economy improvement in many types of vehicles. A survey of all military hybrid peer reviewed publications illustrates that extensive work has been done with regard to their simulation, optimization and controls. All of the literature focuses on three military vehicles: HMMWV, FMTV and HEMMTT, which spans the Class III through Class VIII. However, there are very few publications with respect to military hybrid vehicle hardware[31, 34 and 36], which could be due to cost, proprietary information or the fact that military hybrid vehicle hardware requires more development time than passenger vehicles. Additionally, military vehicles provide unique challenges such as a 60% grade ability, speed on grade, cooling and soft soil mobility.

Many different types of duty cycles were used for the fuel economy investigations. They include time and speed dependant cycles that are defined by the U.S. EPA and distant dependant grade profiles that are defined by the U.S. Army. Both types have duty cycles that represent urban style driving (FUDS, Churchville B) and highway style driving (Federal Highway Cycles, Munson). In addition, some of the publications used a mix so that the fuel economy improvements are reported over a composite duty cycle. While the U.S. Army has tried to define an appropriate military drive cycle, overall there is a lack of an accepted duty cycle to estimate fuel economy improvements such as the FTP 75 used to report miles per gallon for passenger vehicles in the U.S. This could be due to the fact that military threats are constantly changing and it is generally unknown where a military vehicle will be needed.

The fuel economy analyses showed that the Class III vehicle had the greatest potential for fuel economy improvements over an urban cycle and those improvements diminish with composite and highway cycles. Heavier vehicles demonstrate the same trend with respect to drive cycles. In some cases there was even a fuel economy degradation over flatter cycles, such as the Munson cycle. In general, heavier vehicles do not show as much fuel economy potential as the Class III vehicles. Lastly, fuel economy gains are not the only capability that hybrid system can provide a military vehicle. The hybrid system can be used to provide electrical power for soldiers and allow for an improved noise and thermal signature.

Typically, there is a tradeoff between fuel economy and performance, so it is important to understand the performance constraints, such as acceleration and grade ability. Many of the publications used performance constraints in their analysis, but some did not. Furthermore, the analysis where performance constraints were taken into account there was a lack of consistency. Most notably, the 60% grade ability was omitted from most analysis even though this is a requirement for all military vehicles. Therefore, it becomes increasingly difficult to compare and contrast different conclusions.

Conclusions

To fully understand the benefits of a military hybrid vehicle and evaluate the research to date with respect to fuel economy a standard military vehicle using a mix of known military driving conditions. A fuel economy test is a guide that all vehicles are measured by. An example of this is the Federal Test Procedure from 1975 (FTP 75). This is the cycle that is used by all passenger vehicles in the United State to generate the miles per gallon (mpg) that is located on the window sticker of a new vehicle. When a customer reads the sticker mpg they know that this is a number that they may or may not achieve based on driving style and conditions, but it gives them an understanding for how this vehicle compares to other vehicles. Additionally, this standard cycle gives designers and researchers a method to compare their work with the work of others. There is no perfect fuel economy test to represent all driving scenarios and drivers. Furthermore, it is impossible to determine a perfect representative fuel economy drive cycle for a military vehicle because the environments and conditions are constantly changing.

Performance constraints, such as acceleration or grade ability, are parameters that are essential to the development of military vehicles. A hybrid system that can deliver 50% fuel economy improvement but cannot fulfill the acceleration time or grade ability requirements is virtually useless to the military. All of the military performance constraints must be used in the research and development of a military hybrid vehicle; otherwise the work will be viewed as inapplicable in a real work environment and dismissed. These constraints should include traversing a 60% grade, acceleration performance, and speed on grade. The absence of consistent real performance targets and a drive cycles used for analysis could be one of reasons that military hybrids have not been fielded to date.

Future work should include translating many of the concepts surveyed in this paper with regard to controls and optimization of components into a military vehicle prototype vehicle. As with any system, the simulation provides the best case scenario and translating concepts into hardware provides a unique set of challenges such as repeatability, disturbance rejection and response time. This work will provide particular challenges due to the complex nature of the optimization problem, which includes minimizing fuel economy with stringent performance constraints. Furthermore, the optimization problem is dependent not only on the powertrain architecture topology design, i.e. parallel vs. series, batteries vs. ultra capacitors, and component sizing, but also the control system plays a vital role in determining optimal performance. The ever increasing degrees of freedom on a propulsion system demands an ever increasingly complex control system that must not only run real time, but provide the solider with required performance when necessary and optimal efficiency when possible. This control system also has to prolong the life of components and protect them from failing due to fatigue or other causes failures.

Other work could include, exploring how a military hybrid vehicle would perform in an off-road situation and how the hybrid system compares to conventional systems under the same condition. Trying to understand the life cycle cost of a hybrid system in a military environment and how this can be offset with fuel costs. Quantifying the non-fuel economy benefits related to silent mobility and power generation for the warfighter could help the military understand the further payback of fielding a military hybrid vehicle.

Acknowledgements

The authors would like to acknowledge Mike Pozolo, Gus Khalil, U.S. Army RDECOM-TARDEC, and John Beard, Michigan Technological University, for their insight and feedback into to this work.

References

- [1] C.C. Chan, Y.S. Wong, A. Bouscayrol, K. Chen, *Powering Sustainable Mobility: Roadmaps of Electric, Hybrid, and Fuel Cell Vehicles*, Proceedings of the IEEE, Vol. 95, No. 4, April 2009.
- [2] V. Dawood, A. Emadi, *Performance and Fuel Economy Comparative Analysis of Conventional, Hybrid and Fuel Cell Heavy-Duty Transit Buses*, Proceeding of the Vehicular Technology Conference, Vol. 5, pp 3310-3315, October 2003.
- [3] E. Rosenthal, *U.S. Military Orders Less Dependence on Fossil Fuels*, New York Times, October 5, 2010. [4]G. Khalil, *Challenges of Hybrid Electric Vehicles for Military Applications*, Proceedings of the IEEE Vehicle Power and Propulsion Conference, pp. 1-3, September 2009.
- [5] G. Khalil, C. E. Allen, M. Pozolo, *Hybrid-Electric Experimentation and Assessment [HEVEA] Program Supports the Army's Need for Increased Power Demand*, Accelerate, pp. 4-7, April-June 2009.
- [6] C. Williams, *Hybrid-Electric (HE) Drive Knowledge Expanded Through Validation Testing*, Accelerate, pp. 20-21, July-September 2009.
- [7] J.W. Hodgson, W. R. Hamel, C.B. Rutherford, J.S. Armfield, *Design of a Low Production Cost Hybrid HMMWV*, Proceedings of IEEE Digital Avionics Systems Conference, Vol. 2, pp. I46/1, 31 Oct-7 Nov 1998.
- [8] M.M. Freeman, *Hybrid Power An Enabling Technology for Future Combat Systems*, Proceedings of the IEEE Pulsed Power Conference, Vol. 1, pp. 17-22, June 1999.
- [9] R. Crow III, S. P. Cortese, *Dual Use Hybrid Technology for the 21st Century Truck Program*, SAE Paper No. 2000-01-3421, December 2000.
- [10] C. Johnson, L. Dueck, *Hybrid Electric Systems for 20-Ton Platform*, SAE Paper No. 2001-01-2773, November 2001.
- [11] J.S. Ernat, W.G. Harris, T. Trzaska, *Advanced Hybrid Electric Drive (AHED) Technology Demonstrator*, SAE Paper No. 2001-01-2774, November 2001.

- [12] M. A. Kluger, D. Szkubiel, E. A. Bass, *A Dual-Use Hybrid Electric Command and Control Vehicle*, SAE Paper No. 2001-01-2775, November 2001.
- [13] H. Almand, W. Doolittle, G. Klees, *Hybrid Propulsion Truck Platform Dually Developed by the U.S. Army and DaimlerChrysler*, SAE Paper No. 2001-01-2794, November 2001.
- [14] J. M. Paschen, C. Johnson, *Shared Technology/Shared Cost, the Evaluation of the Allison EP-50 Electric Drive for Military and Commercial Vehicles*, SAE Paper No. 2003-01-0271, March 2003.
- [15] P. DiSante, *Hybrid Drive Partnerships Keep the Army on the Right Road*, RDECOM Magazine, June 2003.
- [16] K. Osborn, 3 Firms Win JLTV Contract, Defense News:
- http://www.defensenews.com/story.php?i=3795022&c=AME&s=LAN, October 2009.
- [17] P. Mcleary, Army Taking Another Look at JLTV, Aviation Week:
- http://www.aviationweek.com/aw/generic/story_generic.jsp?channel=aerospacedaily&id=news/asd/20 10/03/03/07.xml, May 2010.
- [18] C. Johnson, *Fuel Savings Design and Engineering Drive the Army's FED Program*, Accelerate: FED Special Edition, pp. 4-9, 2010.
- [19] C. Williams, *Modeling the FED New Concepts, New Techniques*, Accelerate: FED Special Edition, pp. 10-13, 2010.
- [20] M. Seaton, J. Gardini, *Systems Engineering Approach Crucial for the FED Vehicles*, Accelerate: FED Special Edition, pp. 22-27, 2010.
- [21] P. Luskin, R. Berlin, *Systems Engineering Methodology for Fuel Efficiency and its Application to the TARDEC Fuel Efficient Demonstrator (FED) Program*, Proceedings of the NDIA Ground Systems Engineering and Technology Symposium: Systems Engineering Mini-Symposium, August 2010.
- [22] F. An, F. Stodolsky, J.J. Eberhardt, *Fuel and Emission Impacts of Heavy Hybrids*, Argonne National Laboratory, Report Number ANL/ES/CP-98502, 1999.
- [23] F. An, F, Todolsky, A. Vyas, R. Cuenca, J.J. Eberhardt, *Scenario Analysis of Hybrid Class 3-7 Heavy Vehicles*, SAE Paper No. 2000-01-0908, March 2000.
- [24] A. Emadi, K. Rajashekara, S. S. Williamson, S. M. Lukic, *Topological Overview of Hybrid Electric and Fuel Cell Vehicular Power System Architectures and Configurations*, IEEE Transactions on Vehicular Technology, Vol. 54, Issue 3, pp. 763-770, May 2005.
- [25] M. Ehsani, Y. Gao, J. M. Miller, *Hybrid Electric Vehicles: Architecture and Motor Drives,* Proceedings of IEEE, Vol. 95, No. 4, pp. 719-728, April 2007.
- [26] C.C. Chan, *The State of the Art of Electric, Hybrid and Fuel Cell Vehicles*, Proceedings of IEEE, Vol. 95, No. 4, pp. 704-718, April 2007.
- [27] J. Stecki, P. Matheson, Advances in Automotive Hybrid Drives, Proceedings of the 6th JFPS International Symposium on Fluid Power, TSUKUBA. November 2005.
- [28] A. Malikopoulos, Z. Filipi, D. Assanis, *Simulation of an Integrated Starter Alternator (ISA) System for the HMMWV*, SAE Paper No. 2006-01-0442, April 2006.
- [29] Z. Filipi, L. Louca, A. Stefanopoulou, J. Pukrushpan, B. Kittirungsi, H. Peng, Fuel Cell APU for Silent Watch and Mild Electrification of a Medium Tactical Truck, SAE Paper no. 2004-01-1477, March 2004.
- [30] A. I. Antoniou, J. Komyathy, J. Bench, A. Emadi, *Modeling and Simulation of Various Hybrid-Electric Configurations of the High-Mobility Multipurpose Wheeled Vehcile (HMMWV)*, IEEE Transactions on Vehicular Technology, Vol. 56, No. 2, pp. 459-465, March 2007.
- [31] D. Milner, J. Goodell, W. Smith, J. Tzau, M. Pozolo, J. Ueda, *Power System Design Optimization for Tactical Wheeled Vehicles*, Proceedings of the EVS24 International battery Hybrid and Fuel Cell Electric Vehicle Symposium, May 2009.
- [32] Z. Filipi, H. Fathy, J. Hagena, A. Knafl, R. Ahlawat, J. Liu, D. Jung, D. Assanis, H. Peng, J. Stein, *Engine-in-the-Loop Testing for Evaluating Hybrid Propulsion Concepts and Transient Emissions HMMWV Case Study*, SAE Paper No. 2006-01-0443, April 2006.

- [33] A. Filipi, L. Louca, B. Daran, C.C. Lin, U. Yildir, B. Wu, M. Kokkolaras, D. Assanis, H. Peng, P. Papalambros, J. Stein, S. Szkubiel, R. Chapp, *Combined optimization of design and power management of the hydraulic hybrid propulsion system for the 6X6 medium truck*, Int. J. of Heavy Vehicle Systems, Vol. 11, Nos. 3/4, 2004.
- [34] P. Matheson, J. Stecki, *Development and Simulation of a Hydraulic-Hybrid Powertrain for use in Commercial Heavy Vehicles*, SAE 2003-01-3370, November 2003.
- [35] M. Gokasan, S. Bogosyan, D. Goering, *Sliding Mode Based Powertrain Control for Efficiency Improvement in Series Hybrid-Electric Vehicles*, IEEE Transactions on Power Electronics, Vol. 12, No. 3, May 2006.
- [36] H. E. Bargar, J. Li, D. J. Goering, J. H. Lee, *Modeling and Verification of Hybrid Electric HMMWV Performance, Proceeding of the IEEE Industrial Electronics Society 29th Annual Conference*, Vol. 1, p. 939, November 2003.
- [37] C. Liang, W. Weihua, W. Qingnian, *Energy Management Strategy and Parametric Design for Hybrid Electric Military Vehicle*, SAE Paper No. 2003-01-0086, March 2003.
- [38] G. Rizzoni, J. R. Johnson, A. Soliman, C. Huber, C. Cantemir, N. Dembski, P. Pisu, D. Mikesell, L. Serrao, J. Russell, M. Caroll, *Modeling, simulation, and concept design for hybrid-electric medium-size military trucks*, Proceedings of SPIE Vol. 5805, 2005.
- [39] N. Michelena, L. Louca, M. Kokkolaras, C. C. Lin, D. Jung, Z. Filipi, D. Assanis, P. Papalambros, H. Peng, J. Stein, M. Feury, *Design of an Advanced Heavy Tactical Truck: A Target Cascading Case Study*, SAE Paper No. 2001-01-2793, November 2001.
- [40] Y. J. Kim, Z. Filipi, Simulation Study of a Series Hydraulic Hybrid Propulsion System for a Light Truck, SAE Paper No. 2007-01-4151, 2007.
- [41] B. Surampudi, A. Nedungadi, G. Ostrowski, A. Montemayor, H. Gruenewald, *Design and Control Considerations for a Series Heavy Duty Hybrid Hydraulic Vehicle*, SAE Paper no. 2009-01-2717, 2009.
- [42] Drive cycle data: http://www.epa.gov/nvfel/testing/dynamometer.htm
- [43] M. Ducusin, S. Gargies, C. Mi, *Modeling of a Series Hybrid Electric High-Mobility Multipurpose Wheeled Vehicle*, IEEE Transactions on Vehicular Technology, Vol. 56, No. 2, March 2007.
- [44] W. G. Harris, D. L. Ventimeglia, *Will Hybrid electric Propulsion Drive Future Combat Systems*, SAE Paper No. 2002-01-03052, March 2002.
- [45] M. Brudnak, M. Pozolo, M. McGough, T. Mortsfield, A. Shvartsman, R. Romano, *Motion Based Simulation of a Hybrid-Electric HMMWV for Economy Improvements*, SAE Paper No. 2008-01-0775, April 2008.
- [46] Performance Based Purchase Description Hybrid Electric High Mobility Multipurposed Wheeled Vehicle, ATPD 2335, 30 May 2003.
- [47] Vehicle Weight Classifications Emission Standards Reference Guide, Environmental Protection Agency, http://www.epa.gov/otaq/standards/weights.htm.
- [48] K. Chung, A. Reid, D. Fatemi, G. Fryer, *Mulitphysics Simulation and Control Development Environment for Modern Hybrid Electric Drive Military Vehicles*, Proceedings of the 8th World Congress on Computational Mechanics (WCCM8), 5th European Congress on Computational Methods in Applied Sciences and Engineering (ECCOMAS 2008), June 2008.
- [49] D. Desmond, *Power on Call How Auxiliary Power Units Can Extend Mission Times in the Abrams Main Battle Tank*, Accelerate Magazine Energy Efficiency Edition, pp. 37-38, June-August 2011.

Disclaimer: Reference herein to any specific commercial company, product, process, or service by trade name, trademark, manufacturer, or otherwise, does not necessarily constitute or imply its endorsement, recommendation, or favoring by the United States Government or the Department of the Army (DoA). The opinions of the authors expressed herein do not necessarily state or reflect those of the United States Government or the DoA, and shall not be used for advertising or product endorsement purposes.

As the author(s) is(are) not a Government employee(s), this document was only reviewed for export controls, and improper Army association or emblem usage considerations. All other legal considerations are the responsibility of the author and his/her/their employer(s)